

1 **Beyond Equilibrium: Kinetic Thresholds and**
2 **Rheological Feedbacks Create a Potentially Complex**
3 **410 in Slab Regions**

4 **Buchanan Kerswell**¹**John Wheeler**¹**Rene Gassmöller**²**J. Huw Davies**³**Isabel**
5 **Papanagnou**⁴**Sanne Cottaar**⁴

6 ¹Department of Earth, Oceans and Ecological Sciences, University of Liverpool, Liverpool L69 3BX, UK

7 ²GEOMAR Helmholtz Centre for Ocean Research Kiel, Kiel, Germany

8 ³School of Earth and Environmental Sciences, Cardiff University, Park Place, Cardiff, CF10 3AT, UK

9 ⁴Bullard Laboratories, Department of Earth Sciences, University of Cambridge, CB3 0EZ, UK

10 **Key Points:**

- 11 • Plumes produce sharp 410s regardless of reaction rates; slabs show three distinct
12 kinetic regimes controlling discontinuity structure
- 13 • Rheology modulates kinetic effects: strong slabs descend slowly allowing complete
14 reaction; weak slabs descend fast amplifying metastability
- 15 • Seismic observations of 410 structure in subduction zones can constrain reaction
16 rates but require independent rheological constraints

Corresponding author: Buchanan Kerswell, b.kerswell@liverpool.ac.uk

17 **Abstract**

18 The seismic expression of Earth’s 410 km discontinuity varies across tectonic settings,
 19 from sharp, high-amplitude interfaces to broad transitions—patterns that cannot be ex-
 20 plained by equilibrium thermodynamics without invoking large-scale thermal or com-
 21 positional heterogeneities. Laboratory experiments show the olivine \Leftrightarrow wadsleyite phase
 22 transition responsible for the 410 is rate-limited, yet previous numerical studies have not
 23 directly evaluated the sensitivity of 410 structure to kinetic and rheological factors. Here
 24 we investigate these relationships by coupling a grain-scale, interface-controlled olivine
 25 \Leftrightarrow wadsleyite growth model to compressible simulations of mantle plumes and subduct-
 26 ing slabs. We vary kinetic parameters across seven orders of magnitude and quantify the
 27 resulting 410 displacements and widths. Our results reveal an asymmetry between hot
 28 and cold environments. In plumes, high temperatures produce sharp 410s (2–3 km wide)
 29 regardless of kinetics. In slabs, kinetics exert first-order control on 410 structure through
 30 three regimes: (1) quasi-equilibrium conditions producing narrow, uplifted 410s and con-
 31 tinuous slab descent; (2) intermediate reaction rates generating broader, deeper 410s with
 32 metastable olivine wedges resisting downward slab motion; and (3) ultra-sluggish reac-
 33 tion rates causing slab stagnation with re-sharpened, deeply displaced 410s (\lesssim 100 km).
 34 Rheological contrasts modulate these kinetic effects by controlling slab geometry and res-
 35 idence time in the phase transition zone. These findings demonstrate that reaction rates
 36 strongly influence 410 structure in subduction zones, establishing the 410 as a potential
 37 seismological constraint on upper mantle kinetic processes, particularly in cold environ-
 38 ments where disequilibrium effects are amplified.

39 **Plain language summary**

40 Seismic imaging reveals that Earth’s 410 km discontinuity—a boundary in Earth’s man-
 41 tle where olivine transforms into a denser form called wadsleyite—varies significantly,
 42 sometimes appearing sharp and other times as a broad zone. While often explained through
 43 temperature and compositional differences, laboratory experiments show that this min-
 44 eral transformation takes time to complete, suggesting that reaction speed (kinetics) is
 45 important. We simulated rising mantle plumes and descending slabs to explore how ki-
 46 netics and rock strength affect the 410 km discontinuity. Our models reveal striking dif-
 47 ferences: in hot plumes, high temperatures allow fast reactions, maintaining a consis-
 48 tently sharp discontinuity (2–3 km thick). In cold subducting slabs, however, kinetics

49 are critical. Fast reactions produce a narrow, uplifted discontinuity as slabs sink smoothly.
50 Moderate reaction rates create broader, deeper discontinuities with wedges of unreacted
51 olivine that slow downward slab motion. Extremely slow reactions cause slabs to stag-
52 nate with sharp 410 km discontinuities that are shifted downwards by up to 100 km. These
53 findings suggest that observations of the 410 km discontinuity, particularly in subduc-
54 tion zones, could provide valuable constraints on reaction rates deep within Earth's man-
55 tle.

Definition of Symbols

Parameter	Symbol	Unit	Equations
Activation energy	E^*	J mol ⁻¹	15
Activation enthalpy	H^*	J mol ⁻¹	10, 13
Activation factor (rheology)	B	-	18
Activation volume	V^*	m ³ mol ⁻¹	10, 13
Compressibility (reference)	$\bar{\beta}$	Pa ⁻¹	8
Density	ρ	kg m ⁻³	1–4, 7–8
Density (reference)	$\bar{\rho}$	kg m ⁻³	6–8
Density (dynamic)	$\hat{\rho}$	kg m ⁻³	-
Deviatoric stress tensor	σ'	Pa	1, 3
Deviatoric strain rate tensor	$\dot{\epsilon}'$	s ⁻¹	3
Gas constant	R	J mol ⁻¹ K ⁻¹	10, 13, 15–18
Grain size	d	m	-
Gravitational acceleration	g	m s ⁻²	1, 5–6
Growth rate	\dot{x}	m s ⁻¹	9–10, 12
Latent heat	Q_L	J kg ⁻¹	3
Molar entropy	\bar{S}	J mol ⁻¹ K ⁻¹	11
Molar Gibbs free energy	\bar{G}	J mol ⁻¹	11
Molar volume	\bar{V}	m ³ mol ⁻¹	11
Nucleation site factor	N	m ⁻¹	9, 12
Prefactor (growth rate)	Γ	m s ⁻¹ K ⁻¹ ppm _{OH} ⁻ⁿ	10
Prefactor (kinetic)	Z	K s ⁻¹	13
Prefactor (viscosity)	A	Pa s	15–17
Pressure	P	Pa	1, 3, 10, 13
Pressure (reference)	\bar{P}	Pa	6
Pressure (dynamic)	\hat{P}	Pa	8, 11
Reaction rate	$\frac{dX}{dt}, \frac{\partial X}{\partial t}, \dot{X}$	s ⁻¹	12–14
Specific heat capacity (reference)	\bar{C}_p	J kg ⁻¹ K ⁻¹	3, 5

Parameter	Symbol	Unit	Equations
Temperature	T	K	3, 10, 13, 15, 18
Temperature (reference)	\bar{T}	K	5, 16–18
Temperature (dynamic)	\hat{T}	K	8, 11, 16, 18
Thermal conductivity (reference)	\bar{k}	W m ⁻¹ K ⁻¹	3
Thermal expansivity (reference)	$\bar{\alpha}$	K ⁻¹	3, 5, 8
Time	t	s	2–4, 9, 12–14
Velocity	\vec{u}	m s ⁻¹	2–4, 14
Viscosity	η	Pa s	15–16, 18
Viscosity (reference)	$\bar{\eta}$	Pa s	17–18
Volume fraction	X	-	9, 12–14
Water content	C_{OH}	ppm	10
Water content exponent	n	-	10

57 1 Introduction

58 Earth’s mantle transition zone hosts two prominent seismic discontinuities near 410
 59 and 660 km depth, attributed to polymorphic phase transitions of olivine (Katsura et
 60 al., 2004; Ringwood, 1975). While these discontinuities are observed globally, their de-
 61 tailed seismic characteristics—depth, sharpness, amplitude, and lateral continuity—vary
 62 substantially between tectonic settings (Deuss, 2009; Fukao & Obayashi, 2013; Lawrence
 63 & Shearer, 2008; Schmerr & Garnero, 2007). Some regions display sharp, high-amplitude
 64 reflectors consistent with abrupt mineralogical boundaries, while others exhibit broad,
 65 weakened, or laterally variable signals. Such heterogeneity cannot be explained by equi-
 66 librium thermodynamics alone, which relates discontinuity topography mainly to temperature-
 67 dependent phase boundaries (e.g., Cottar & Deuss, 2016; Jenkins, Cottar, White, &
 68 Deuss, 2016). Additional physical processes, including reaction kinetics and dynamic pres-
 69 sure effects (Faccenda & Dal Zilio, 2017; Rubie & Ross II, 1994), or compositional het-
 70 erogeneities, including variations in water content (S. Karato, 2011; Smyth, 1987; Smyth
 71 & Frost, 2002) or bulk composition (Glasgow, Zhang, Schmandt, Zhou, & Zhang, 2024;
 72 Goes, Yu, Ballmer, Yan, & van der Hilst, 2022; Saikia, Frost, & Rubie, 2008; Schmerr
 73 & Garnero, 2007; Tauzin, Kim, & Kennett, 2017) likely contribute to observed variabil-
 74 ity.

75 Laboratory studies demonstrate that the olivine \Leftrightarrow wadsleyite phase transition at
 76 410 km depth (the “410”) occurs over finite time scales rather than instantaneously, with
 77 kinetics governed by temperature, pressure, water content, bulk chemical composition,
 78 grain size, and microstructural evolution (Hosoya, Kubo, Ohtani, Sano, & Funakoshi,
 79 2005; Kubo, Ohtani, & Funakoshi, 2004; Ledoux et al., 2023; Liu, Kerschhofer, Mosen-
 80 felder, & Rubie, 1998; Perrillat et al., 2013; Rubie & Ross II, 1994). In cold subducting
 81 slabs, sluggish reaction rates can allow metastable olivine to persist tens of kilometers
 82 below its thermodynamic stability limit, promoting slab stagnation and potentially trig-
 83 gering deep earthquakes via transformational faulting (H. Green & Houston, 1995; Ishii
 84 & Ohtani, 2021; Kirby, Stein, Okal, & Rubie, 1996; Ohuchi et al., 2022; Rubie & Ross II,
 85 1994; Sindhusuta, Chi, Foster, Officer, & Wang, 2025). In hot upwellings, slow kinetics
 86 may broaden and uplift the discontinuity, possibly explaining reduced seismic amplitudes
 87 beneath some hotspots (Chambers, Deuss, & Woodhouse, 2005). However, published ki-
 88 netic models remain poorly constrained, with parameters spanning several orders of mag-

89 nitude (e.g., Hosoya et al., 2005), leaving the effects of micro-scale kinetic processes on
90 flow dynamics and seismic observables ambiguous.

91 Bridging the gap between laboratory-derived kinetic rate laws and mantle-scale seis-
92 mic observations requires numerical models that couple reaction kinetics to realistic treat-
93 ments of mantle convection. Previous modeling efforts have demonstrated that kinet-
94 ics can strongly influence mantle flow (Agrusta, Goes, & Van Hunen, 2017; Däßler & Yuen,
95 1996; Däßler, Yuen, Karato, & Riedel, 1996; Faccenda & Dal Zilio, 2017; Guest, Schu-
96 bert, & Gable, 2004; Schmeling, Monz, & Rubie, 1999), but investigations quantifying
97 the sensitivity of 410 structure to kinetic parameters remain limited. Moreover, most prior
98 studies impose kinematic restrictions and/or employ simplified treatments of compress-
99 ibility or kinetic rate laws that may inadequately capture feedbacks between kinetically
100 controlled phase transitions and flow dynamics. Additionally, the role of rheology in mod-
101 ulating kinetic effects through its control on slab geometry and descent rate has not been
102 thoroughly explored.

103 This study aims to clarify these issues by implementing a grain-scale interface-controlled
104 olivine \Leftrightarrow wadsleyite growth model (after Hosoya et al., 2005) within compressible man-
105 tle flow simulations using the open-source geodynamic modeling software ASPECT. We
106 systematically explore how reaction kinetics and rheological strength jointly influence
107 410 structure and address three specific questions:

- 108 1. How do kinetic factors impact flow dynamics and shape the 410 in hot versus cold
109 environments?
- 110 2. How do viscosity contrasts modulate these kinetic effects?
- 111 3. Can seismic observations of 410 structure constrain effective kinetic and rheolog-
112 ical parameters?

113 To investigate these questions, we analyze a suite of numerical experiments vary-
114 ing kinetic parameters across seven orders of magnitude. For each experiment, we test
115 a range of viscosity contrasts and quantify 410 displacement and width, enabling direct
116 comparisons with seismological observations. Our results establish quantitative relation-
117 ships between reaction rates, rheological strength, flow dynamics, and 410 structure, demon-
118 strating that realistic treatment of reaction kinetics is essential for accurately modeling
119 subduction dynamics and interpreting seismic structures.

2 Methods

2.1 Governing Equations for Compressible Mantle Flow

Mantle flow is simulated using the finite-element geodynamic code ASPECT (v3.0.0, Bangerth et al., 2024a, 2024b; Clevenger & Heister, 2021; Fraters, 2020; Fraters, Thieulot, van den Berg, & Spakman, 2019; Gassmüller, Lokavarapu, Heien, Puckett, & Bangerth, 2018; Heister, Dannberg, Gassmüller, & Bangerth, 2017; Kronbichler, Heister, & Bangerth, 2012) to find the velocity \vec{u} , pressure P , and temperature T fields that satisfy the following equations:

$$\nabla P - \nabla \cdot \sigma' = \rho g \quad (1)$$

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{u}) = 0 \quad (2)$$

$$\rho \bar{C}_p \left(\frac{\partial T}{\partial t} + \vec{u} \cdot \nabla T \right) - \nabla \cdot (\bar{k} \nabla T) = \sigma' : \dot{\epsilon}' + \bar{\alpha} T (\vec{u} \cdot \nabla P) + Q_L \quad (3)$$

where σ' is the deviatoric stress tensor, ρ is density, g is gravitational acceleration, t is time, \bar{C}_p , \bar{k} , $\bar{\alpha}$ are the reference specific heat capacity, thermal conductivity, and thermal expansivity, respectively (see Section 2.2.1), and Q_L is the latent heat released or absorbed during phase transitions. Equations 1 and 2 together describe the buoyancy-driven flow of an isotropic fluid with negligible inertia and Equation 3 describes the conduction, advection, and production (or consumption) of thermal energy (Schubert, Turcotte, & Olson, 2001). Note that the pressure P in this context is equal to the mean normal stress and is positive under compression: $P = -\frac{\sigma_{xx} + \sigma_{yy} + \sigma_{zz}}{3}$.

The compressible form of the continuity equation (Equation 2) is essential for capturing the full coupling between density changes, pressure and temperature (PT) variations, and kinetically-controlled phase transitions. This is in contrast to simplified formulations such as the Boussinesq approximation or anelastic liquid approximation, which either neglect the time derivative of density ($\frac{\partial \rho}{\partial t}$) entirely or impose restrictions on where density variations can appear in the governing equations (Gassmüller, Dannberg, Bangerth, Heister, & Myhill, 2020). By retaining $\frac{\partial \rho}{\partial t}$, the compressible continuity equation enables density changes from kinetically-controlled phase transitions to influence the flow field

144 anywhere within the model domain—not just through equilibrium thermodynamics, but
 145 through time-dependent reaction progress. This bidirectional coupling between flow dy-
 146 namics and reaction kinetics is critical for accurately simulating systems where phase
 147 transitions occur over finite timescales comparable to advective timescales.

148 To solve Equation 2 numerically we adopt the *projected density approximation* (PDA,
 149 Gassmüller et al., 2020), which reformulates the continuity equation by applying the prod-
 150 uct rule to $\nabla \cdot (\rho \vec{u})$ and multiplying both sides by $\frac{1}{\rho}$:

$$\frac{1}{\rho} \frac{\partial \rho}{\partial t} + \nabla \cdot \vec{u} + \left(\frac{1}{\rho} \nabla \rho \right) \cdot \vec{u} = 0 \quad (4)$$

151 The projected density field $\rho(T, P, X)$ varies with temperature, pressure, and re-
 152 action progress, ensuring that local density changes arising from both PT variations and
 153 phase transitions influence the flow through buoyancy as well as volumetric expansion
 154 and compression. The phase transitions themselves are modeled using a separate kinetic
 155 rate law (described in Section 2.2.3.2), which determines the reaction progress X based
 156 on local thermodynamic and kinetic conditions. This makes the PDA ideally suited for
 157 our numerical experiments, which incorporate density changes due to the olivine \Leftrightarrow wad-
 158 sleyite phase transition.

159 2.2 Numerical Setup

160 2.2.1 Adiabatic Reference Conditions

161 To ensure numerical convergence, we initialized our ASPECT simulations with rea-
 162 sonable estimates of the pressure-temperature (PT) fields and material properties in Earth’s
 163 upper mantle. We began by evaluating entropy changes over a PT range of 1573–1973
 164 K and 0.001–25 GPa (Figure 1) using the Gibbs free energy minimization software Per-
 165 ple_X (v.7.0.9, Connolly, 2009). We assumed a dry pyrolitic bulk composition after D. Green,
 166 Jaques, and Hibberson (1979) and phase equilibria were evaluated in the Na₂O-CaO-
 167 FeO-MgO-Al₂O₃-SiO₂ (NCFMAS) chemical system with thermodynamic data and so-
 168 lution models of Stixrude and Lithgow-Bertelloni (2022). Equations of state were included
 169 for solid solution phases: olivine, plagioclase, spinel, clinopyroxene, wadsleyite, ringwood-
 170 ite, perovskite, ferropericlase, high-pressure C2/c pyroxene, orthopyroxene, akimotoite,
 171 post-perovskite, Ca-ferrite, garnet, and Na-Al phase.

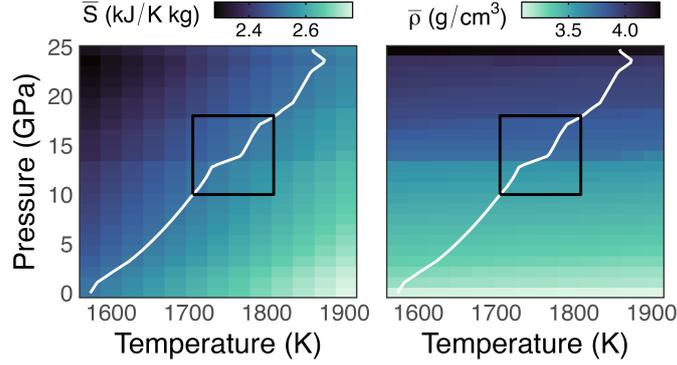


Figure 1: Entropy (left) and density (right) changes in Earth’s upper mantle under thermodynamic equilibrium and hydrostatic stress conditions. Material properties were computed with *Perple_X* using the equations of state and thermodynamic data of *Stixrude* and *Lithgow-Bertelloni* (2022). The black box indicates the approximate PT range of our ASPECT simulations, while the white line indicates the isentropic adiabat used to calculate reference material properties.

172 We then determined the mantle adiabat by applying the Newton-Raphson algo-
 173 rithm to find temperatures corresponding to each pressure that maintain constant en-
 174 tropy (white line in Figure 1). Material properties were evaluated at each PT point along
 175 the isentrope to construct the adiabatic reference conditions shown in Figure 2. These
 176 reference conditions serve three main purposes: 1) initializing the PT fields and mate-
 177 rial properties in our ASPECT simulations (see Section 2.2.2), 2) updating the mate-
 178 rial model during the simulations (see Section 2.2.3), and 3) serving as a basis for com-
 179 puting “dynamic” quantities, such as the dynamic temperature $\hat{T} = T - \bar{T}$, dynamic
 180 pressure $\hat{P} = P - \bar{P}$, and dynamic density $\hat{\rho} = \rho - \bar{\rho}$, that quantify how much the ap-
 181 proximate numerical solution deviates from the adiabatic reference conditions.

182 **2.2.2 Initialization and Boundary Conditions**

183 We setup our ASPECT simulations within a 900×600 km rectangular model do-
 184 main, initialized with pure Mg olivine and wadsleyite (Figure 3). “Surface” PT condi-
 185 tions of 10 GPa and 1706 K were applied at the top boundary such that the olivine \Leftrightarrow
 186 wadsleyite transition occurs at approximately 130–140 km from the top boundary. The

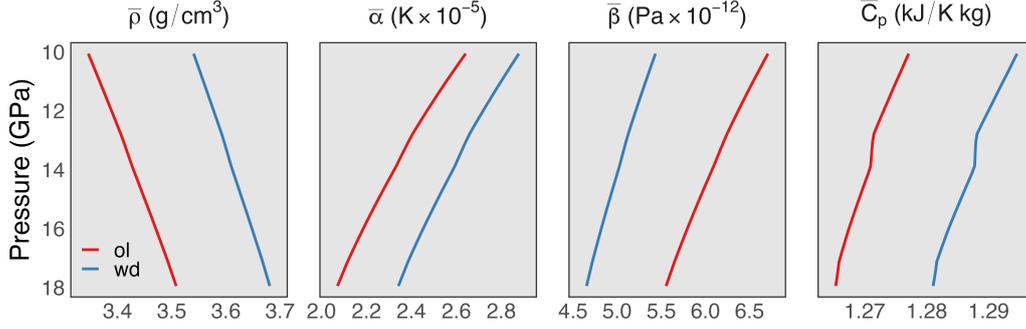


Figure 2: Reference material properties used in our ASPECT simulations. Profiles were computed using the BurnMan software (Cottaar et al., 2014; Myhill et al., 2023) and were based on the equations of state and thermodynamic data of Stixrude and Lithgow-Bertelloni (2022) for pure Mg olivine (ol) and wadsleyite (wd).

187 initial adiabatic PT profiles were computed by numerically integrating the following equa-
 188 tions:

$$\frac{d\bar{T}}{dy} = \frac{\bar{\alpha} \bar{T} g}{\bar{C}_p} \quad (5)$$

$$\frac{d\bar{P}}{dy} = \bar{\rho} g \quad (6)$$

189 where the material properties $\bar{\rho}$, $\bar{\alpha}$, and \bar{C}_p were determined from the adiabatic ref-
 190 erence conditions shown in Figure 2.

191 For the initial temperature field, thermal anomalies with amplitudes of ± 500 K
 192 were superimposed on the adiabatic temperature profile. These anomalies were defined
 193 as smooth linear features with Gaussian cross-sections (15 km half-width) and tanh ta-
 194 pered ends (5 km taper length) to avoid sharp discontinuities. Slabs extended 100 km
 195 horizontally and 100 km downward from the top boundary; plumes extended 450 km up-
 196 ward from the bottom boundary. Velocity boundary conditions prescribed constant in-
 197 flow of 5 cm/yr parallel to the thermal anomalies, tapering smoothly to zero at the ther-
 198 mal anomaly edges with the same Gaussian profile. Zero horizontal velocities were im-
 199 posed at the side boundaries ($\vec{u}_x = 0$). The full functional form of the Gaussian-tanh

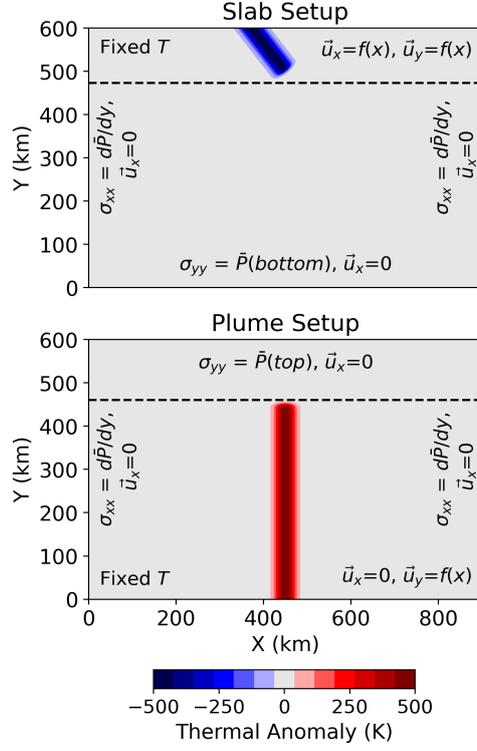


Figure 3: Initial setup for slab (top) and plume (bottom) simulations. The top boundary has a constant “surface” PT of 10 GPa and 1706 K such that the olivine \Leftrightarrow wadsleyite phase transition (dashed line) occurs at 130–140 km from the top boundary. Thermal anomalies with Gaussian profiles were superimposed on top of the initial adiabatic temperature profile and remained fixed at the inflow boundary. Constant inflow velocities of 5 cm/yr were prescribed parallel to the thermal anomalies. Normal tractions equal to the initial lithostatic pressure profile were enforced on the left, right, and open boundaries to ensure that outflows are driven only by dynamic pressures.

200 thermal anomalies and velocity boundary conditions are available within the accompa-
 201 nyng data repository (see Data Availability statement for details).

202 Stress boundary conditions on the left and right boundaries enforced a normal trac-
 203 tion equal to the lithostatic pressure profile computed in Equation 6. No tangential (shear)
 204 stresses were applied to the side boundaries, so they approximated impermeable, free-
 205 slip surfaces under hydrostatic confinement. Open boundaries (bottom for slabs, top for
 206 plumes) were assigned a constant normal traction equal to the initial lithostatic pres-
 207 sure at the respective boundary $\sigma_{yy} = \bar{P}(y)$. These stress conditions allow outflow to
 208 occur freely at the top or bottom boundaries (for plumes versus slabs), driven only by
 209 dynamic pressure variations associated with convection and/or volume changes during
 210 the olivine \Leftrightarrow wadsleyite phase transition.

211 **2.2.3 Material Model**

212 *2.2.3.1 Material Properties* Material properties were updated during our AS-
 213 PECT simulations by referencing the adiabatic reference conditions shown in Figure 2.
 214 Except for density, material properties received no PT corrections, effectively assuming
 215 that deviations from the adiabatic reference conditions were negligible. For density, how-
 216 ever, we applied a dynamic PT correction through a first-order Taylor expansion (Gassmüller
 217 et al., 2020; Jarvis & Mckenzie, 1980):

$$\rho \approx \bar{\rho} + \left(\frac{\partial \bar{\rho}}{\partial P} \right)_T \Delta P + \left(\frac{\partial \bar{\rho}}{\partial T} \right)_P \Delta T \quad (7)$$

218 Equation 7 is rewritten using standard thermodynamic relations $\beta = \frac{1}{\rho} \left(\frac{\partial \rho}{\partial P} \right)_T$
 219 and $\alpha = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_P$ to obtain the expression:

$$\rho \approx \bar{\rho} \left(1 + \bar{\beta} \hat{P} - \bar{\alpha} \hat{T} \right) \quad (8)$$

220 where $\bar{\rho}$, $\bar{\beta}$, $\bar{\alpha}$, are the adiabatic reference density, compressibility, and thermal ex-
 221 pansivity, respectively, and $\Delta P = \hat{P} = P - \bar{P}$ and $\Delta T = \hat{T} = T - \bar{T}$ are the dynamic
 222 PT. Note that the reference thermal conductivity $\bar{k} = 4.0 \text{ W m}^{-1}\text{K}^{-1}$ is constant in all
 223 our numerical experiments.

224 *2.2.3.2 Reaction Kinetics* The kinetics of the olivine \leftrightarrow wadsleyite phase tran-
 225 sition were governed entirely by interface-controlled growth, as nucleation was assumed
 226 to saturate rapidly and did not limit the reaction (Cahn, 1956). Following Faccenda and
 227 Dal Zilio (2017), the transformed volume fraction is given by:

$$X = 1 - \exp(-N \dot{x} t) \quad (9)$$

228 where X is the volume fraction of the product phase (olivine or wadsleyite), N is
 229 a geometric factor that accounts for nucleation sites, \dot{x} is the growth rate, and t is the
 230 elapsed time after site saturation. For inter-crystalline grain-boundary controlled growth,
 231 $N = 6.67/d$, where d is grain size.

232 Since we assumed interface-controlled growth kinetics, the following expression de-
 233 termined the overall reaction rate (Hosoya et al., 2005):

$$\dot{x} = \Gamma T C_{\text{OH}}^n \exp\left(-\frac{H^* + PV^*}{RT}\right) \left(1 - \exp\left[-\frac{\Delta G}{RT}\right]\right) \quad (10)$$

234 where Γ is the growth rate prefactor, C_{OH} is the concentration of water in the re-
 235 actant phase, n is the water content exponent, H^* is activation enthalpy, V^* is activa-
 236 tion volume, P is pressure, T is temperature, R is the gas constant, and ΔG is the Gibbs
 237 free energy difference between olivine and wadsleyite, which is approximated by:

$$\Delta G \approx \Delta \bar{G} + \hat{P} \Delta \bar{V} - \hat{T} \Delta \bar{S} \quad (11)$$

238 where $\Delta \bar{G}$, $\Delta \bar{V}$, and $\Delta \bar{S}$ are the molar Gibbs free energy, volume, and entropy dif-
 239 ferences between olivine and wadsleyite along the adiabatic reference profile (Figure 4),
 240 respectively, and \hat{P} and \hat{T} are the dynamic PT.

241 This formulation represents a significant thermodynamic simplification: we define
 242 Gibbs free energy based on mean normal stress (pressure), whereas our simulations in-
 243 volve non-hydrostatic stress conditions where deviatoric stresses and normal stresses at
 244 individual grain interfaces directly influence reaction pathways and chemical potentials
 245 (Wheeler, 2015, 2020). While mean stress can provide a reasonable approximation un-
 246 der certain conditions (Wheeler, 2020), a rigorous treatment would require stress-dependent

247 chemical potentials that account for the full stress tensor’s influence on phase stability
 248 and reaction kinetics.

249 Setting aside these important microstructural effects for now, the time evolution
 250 of the olivine \Leftrightarrow wadsleyite phase transition is fully described by the interplay of pres-
 251 sure, temperature, and kinetic parameters applied to the interface-controlled growth model,
 252 without explicit consideration of nucleation kinetics (Faccenda & Dal Zilio, 2017; Hosoya
 253 et al., 2005). The macro-scale olivine \Leftrightarrow wadsleyite reaction rate was therefore computed
 254 by taking the time derivative of Equation 9:

$$\frac{dX}{dt} = \dot{X} = N \dot{x} (1 - X) \quad (12)$$

255 Since all of the kinetic parameters N , Γ , and C_{OH}^n ultimately scale the reaction rate
 256 (Equations 10–12), varying them independently adds little scientific value. Instead, we
 257 simplified our numerical implementation of Equation 12 by combining the parameters
 258 N , Γ , and C_{OH}^n into a single kinetic prefactor $Z = \frac{6.67}{d} \Gamma C_{\text{OH}}^n$. Thus, the full expres-
 259 sion for the reaction rate became:

$$\dot{X} = Z T \exp\left(-\frac{H^* + PV^*}{RT}\right) \left(1 - \exp\left[-\frac{\Delta G}{RT}\right]\right) (1 - X) \quad (13)$$

260 The range of kinetic prefactors Z used in our numerical experiments (3.0e0–7.0e7
 261 K s⁻¹) was determined by holding $\Gamma = \exp(-18)$ m s⁻¹ K⁻¹ ppm_{OH}⁻ⁿ, $H^* = 274$ kJ mol⁻¹,
 262 $V^* = 3.0\text{e-}6$ m³ mol⁻¹, and $n = 3.2$ constant, while varying water content C_{OH} from 50–
 263 5000 ppm and grain size d from 1–10 mm. These water contents and grain sizes are con-
 264 sistent with the experimental conditions of Hosoya et al. (2005), previous numerical stud-
 265 ies of metastable olivine wedges (Rubie & Ross II, 1994), and typical grain sizes of up-
 266 per mantle xenoliths (~3–10 mm, S. Karato, 2008; S.-I. Karato, 1984). Thus, our exper-
 267 iments approximate kinetic conditions ranging from slow kinetics in dry rocks with large
 268 grain sizes (50 ppm OH; 10 mm; $Z = 3.0\text{e}0$ K s⁻¹) to fast kinetics in hydrated rocks with
 269 small grain sizes (5000 ppm OH; 1 mm; $Z = 7.0\text{e}7$ K s⁻¹).

270 *2.2.3.3 Operator Splitting* Since the reaction rate \dot{X} was faster than the advec-
 271 tion timescale in our ASPECT simulations, we employed a first-order operator splitting
 272 scheme to decouple advection from interface-controlled olivine \Leftrightarrow wadsleyite growth ki-

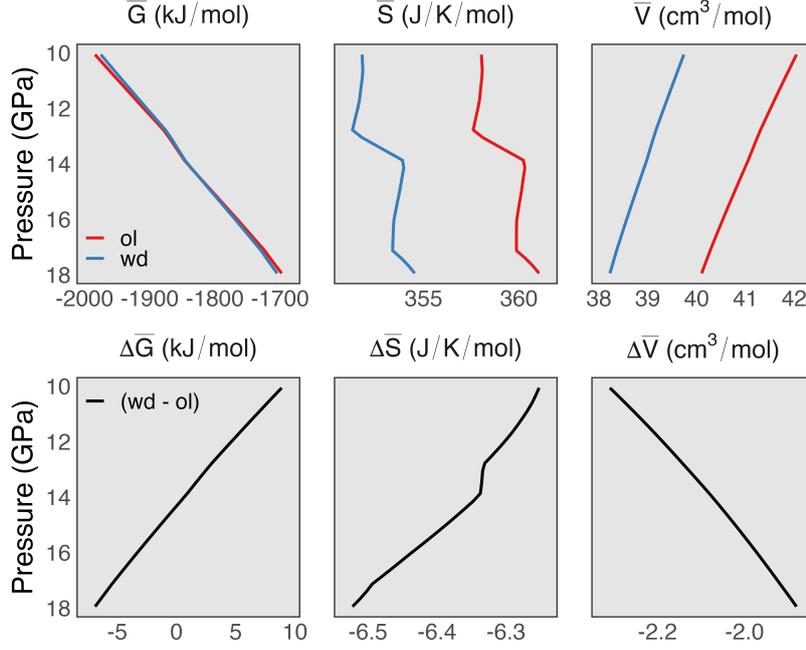


Figure 4: Reference thermodynamic properties used in our ASPECT simulations. Profiles were computed using the same methods as described in Figure 2 (see Section 2.2.1).

273 netics. In this approach, the transformed volume fraction X was updated in two sequen-
 274 tial steps within each overall time step Δt :

$$\frac{\partial X}{\partial t} + \vec{u} \cdot \nabla X = 0 \quad (14)$$

- 275 1. **Reaction step:** Starting from X^t , the reaction rate equation (Equation 13) was
 276 integrated forward in time over the full advection timestep Δt , yielding an inter-
 277 mediate composition X^* . This integration was performed using a sequence of in-
 278 ternally determined reaction substeps $\delta t \leq \Delta t$, such that the reaction operator
 279 was applied repeatedly until the cumulative integration time reached Δt .
- 280 2. **Advection step:** Starting from X^* , the material transport term ($\vec{u} \cdot \nabla X$) in Equa-
 281 tion 14 was solved over the advection time interval Δt , neglecting phase changes,
 282 to obtain the updated composition X^{t+1} .

283 In our simulations, the reaction step was solved using the ARKODE package of the
 284 SUNDIALS library (Hindmarsh et al., 2005; Reynolds, Gardner, Woodward, & Chinomona,

285 2023), which employs an adaptive-step additive Runge-Kutta method (Bangerth et al.,
 286 2024a). The reaction substep size δt was determined dynamically by ARKODE to sat-
 287 isfy a specified relative tolerance during the reaction step (set to 10^{-6} in this study). As
 288 a result, the reaction operator was subcycled as needed within each global timestep Δt ,
 289 ensuring that fast solid-state reaction kinetics were accurately captured without impos-
 290 ing overly restrictive global timesteps.

291 **2.2.4 Rheological Model**

292 We use a temperature-dependent viscosity following an Arrhenius law:

$$\eta = A \exp\left(\frac{E^*}{RT}\right) \quad (15)$$

293 with viscosity prefactor A , activation energy E^* , gas constant R , and absolute tem-
 294 perature T , which is decomposed into an adiabatic reference temperature \bar{T} and a per-
 295 turbation \hat{T} , $T = \bar{T} + \hat{T}$. Linearizing the Arrhenius relation through a first-order Tay-
 296 lor expansion about \bar{T} yields:

$$\eta \approx A \exp\left(\frac{E^*}{R\bar{T}}\right) \exp\left(-\frac{E^* \hat{T}}{R\bar{T}^2}\right) \quad (16)$$

297 By defining a reference background viscosity as:

$$\bar{\eta} = A \exp\left(\frac{E^*}{R\bar{T}}\right) \quad (17)$$

298 we arrive at a rheological model where viscosity varies exponentially with thermal
 299 perturbations about an adiabatic reference profile:

$$\eta \approx \bar{\eta} \exp\left(-B \frac{\hat{T}}{\bar{T}}\right) \quad B = \frac{E^*}{R\bar{T}} \quad (18)$$

300 In our simulations, we prescribed a uniform background viscosity $\bar{\eta} = 10^{21}$ Pa s through-
 301 out the upper mantle (e.g., S. Karato, 2008; Ranalli, 1995), implicitly assuming that E^*
 302 was temperature-dependent and varied slightly with depth (Equation 17). We varied the
 303 rheological activation factor B between 2 (low thermal sensitivity) and 10 (high ther-
 304 mal sensitivity). For our prescribed thermal anomalies of $\hat{T} = \pm 500$ K, these B values

305 correspond to approximately 2–20× stronger slabs or 2–20× weaker plumes relative to
 306 the background mantle for $B = 2$ and 10, respectively. Thus, our numerical experiments
 307 explore a range of viscosity contrasts between thermal anomalies and background adi-
 308 abatic reference conditions, with the exponential rheological model creating symmetric
 309 viscosity variations for heating and cooling.

310 ***2.2.5 Numerical Stabilization of Dynamic Pressure Oscillations***

311 A significant numerical limitation emerges from the coupled feedback between our
 312 kinetic rate law (Equations 9–13) and the buildup of dynamic pressure in the fully com-
 313 pressible continuity equation (Equation 2). At sufficiently high rheological contrasts (B
 314 $\gtrsim 4$), cold slabs develop internal dynamic pressures that can exceed several hundred MPa.
 315 These dynamic pressure perturbations accelerate the forward reaction (through the Gibbs
 316 free energy term in Equation 13), causing rapid local density changes. These density changes
 317 then alter the pressure field through the coupled continuity and momentum equations
 318 (Equations 1–2), which in turn drives the reverse reaction. This positive feedback loop
 319 manifests as spurious pressure waves propagating through the slab interior.

320 To address this issue, we adopt an approach similar to Gassmüller et al. (2020) and
 321 exclude the dynamic pressure contribution from the Gibbs free energy calculation (Equa-
 322 tion 11) while retaining it in the Arrhenius term in Equation 13 and density formula-
 323 tion (Equation 8). In practice, this means replacing $\Delta G \approx \Delta \bar{G} + \hat{P} \Delta \bar{V} - \hat{T} \Delta \bar{S}$ with
 324 $\Delta G \approx \Delta \bar{G} - \hat{T} \Delta \bar{S}$ in our kinetic rate law. As discussed by Gassmüller et al. (2020),
 325 this approximation is justified because density variations from dynamic pressure are typ-
 326 ically small compared to those from compositional heterogeneities and temperature vari-
 327 ations in mantle convection. However, this treatment does introduce a limitation: in sce-
 328 narios where dynamic pressure effects dominate over thermal and compositional contri-
 329 butions, such as in regions with extreme viscosity contrasts or near phase boundaries with
 330 large $\Delta \bar{V}$, our kinetic model may underestimate the thermodynamic driving force for phase
 331 transitions. Nevertheless, this compromise ensures numerical stability while preserving
 332 the essential physics of kinetically controlled phase transitions coupled to compressible
 333 flow.

3 Results

3.1 Simulation Snapshots: Slabs and Plumes

Figures 5 and 6 illustrate how reaction rates impact dynamic flow patterns and shape the 410 discontinuity. These snapshots, taken after 100 Ma of evolution, provide visual context for the quantitative analysis in Section 3.2.

In slab simulations, ultra-sluggish kinetics (Figure 5: top row) allow metastable olivine to persist deep into the transition zone. This inhibition causes the slab to stagnate and pond, depressing the 410. Within the cold, metastable olivine region, Gibbs free energy accumulates and wadsleyite saturation remains low until the thermodynamic driving force overcomes kinetic barriers. Once this threshold is reached, the olivine \leftrightarrow wadsleyite reaction rapidly completes, producing a sharp 410 that is displaced downwards by tens of kilometers.

At intermediate reaction rates (Figure 5: middle row), the olivine \leftrightarrow wadsleyite reaction still lags but is fast enough to limit widespread olivine metastability and avoid total slab stagnation. The resulting 410 is broad and diffuse, as density and seismic velocity contrasts gradually fade with depth. This moderately-sluggish kinetic regime produces complex 410 structures through intermediate reaction rates, incomplete slab stagnation, and deflected flow patterns. However, when reaction rates are sufficiently fast to maintain quasi-equilibrium conditions (Figure 5: bottom row), the 410 sharpens and shifts upwards as expected from equilibrium thermodynamics. Under this fast kinetic regime, rapid wadsleyite growth within the slab allows continuous slab descent through the 410 without hesitation.

In plume simulations, thermal effects dominate mantle flow dynamics and 410 structure. Even under ultra-sluggish kinetics (Figure 6: top row), the high temperatures of upwellings prevent significant wadsleyite metastability. The olivine \leftrightarrow wadsleyite transition proceeds rapidly, maintaining thin, sharp 410 interfaces and strong density and seismic contrasts. Although ultra-sluggish kinetics slightly broaden and uplift the 410, reducing buoyancy contrasts, plume structures remain vertically coherent across the full range of tested kinetic prefactors Z (Figure 6).

Altogether, these simulations demonstrate that in cold environments, kinetics strongly influence slab dynamics and control whether the 410 appears as a diffuse, low-amplitude

365 feature or as a sharp, high-contrast seismic boundary. In contrast, thermal effects dom-
 366 inate in hot plume environments, producing stable, sharply defined 410s that are largely
 367 independent of tested kinetic prefactors.

368 **3.2 Structure of the 410: Displacement and Width**

369 Figure 7 summarizes the quantitative relationships between 410 structure and the
 370 maximum reaction rate \dot{X}_{\max} evaluated in slab and plume simulations after 100 Ma of
 371 evolution. The results reveal fundamentally different responses of plumes and slabs to
 372 reaction kinetics. See the Supplementary Information for the full set of experimental re-
 373 sults and technical details describing the 410 structural measurements.

374 In plume simulations, the 410 shows little dependence on \dot{X}_{\max} . Its structure re-
 375 mains nearly constant across seven orders of magnitude variation in \dot{X}_{\max} , with consis-
 376 tent displacements of 24 km and widths between 2–9 km. The only exception is a few
 377 ultra-sluggish kinetic models where displacements decrease to 18–21 km and widths in-
 378 crease to 12–21 km. The weak dependence of 410 structure on \dot{X}_{\max} reflects the strong
 379 thermal control of the reaction front in upwellings, where high temperatures promote rapid
 380 wadsleyite \leftrightarrow olivine transition—maintaining a sharp discontinuity regardless of the ki-
 381 netic prefactor Z applied to the interface-controlled olivine \leftrightarrow wadsleyite growth model
 382 (Equation 13). Similarly, variations in rheological strength contrast (controlled by the
 383 B parameter in Equation 18) produce negligible changes to plume morphology or 410
 384 structure, as the thermally-dominated behavior is largely insensitive to viscosity vari-
 385 ations (see Supplementary Information for examples).

386 In slab simulations, the 410 exhibits distinct structural changes across three kinetic
 387 regimes. At high reaction rates ($Z \gtrsim 1.8e5 \text{ K s}^{-1}$; $\dot{X}_{\max} \gtrsim 2.2 \text{ Ma}^{-1}$), the olivine \leftrightarrow wad-
 388 sleyite transition remains near thermodynamic equilibrium, producing a narrow 410 (\lesssim
 389 10 km), displaced 27–39 km upwards within the slab’s inner core. As \dot{X}_{\max} decreases ($2.0e2$
 390 $\lesssim Z \lesssim 1.8e5 \text{ K s}^{-1}$; $0.07 \lesssim \dot{X}_{\max} \lesssim 2.2 \text{ Ma}^{-1}$), the 410 deepens and widens, approxi-
 391 mating a log-linear relationship where reductions in \dot{X}_{\max} progressively broaden the re-
 392 action front. This intermediate kinetic regime corresponds to a partially inhibited olivine
 393 \leftrightarrow wadsleyite phase transition that proceeds slowly, hindering downward flow without
 394 complete slab stagnation.

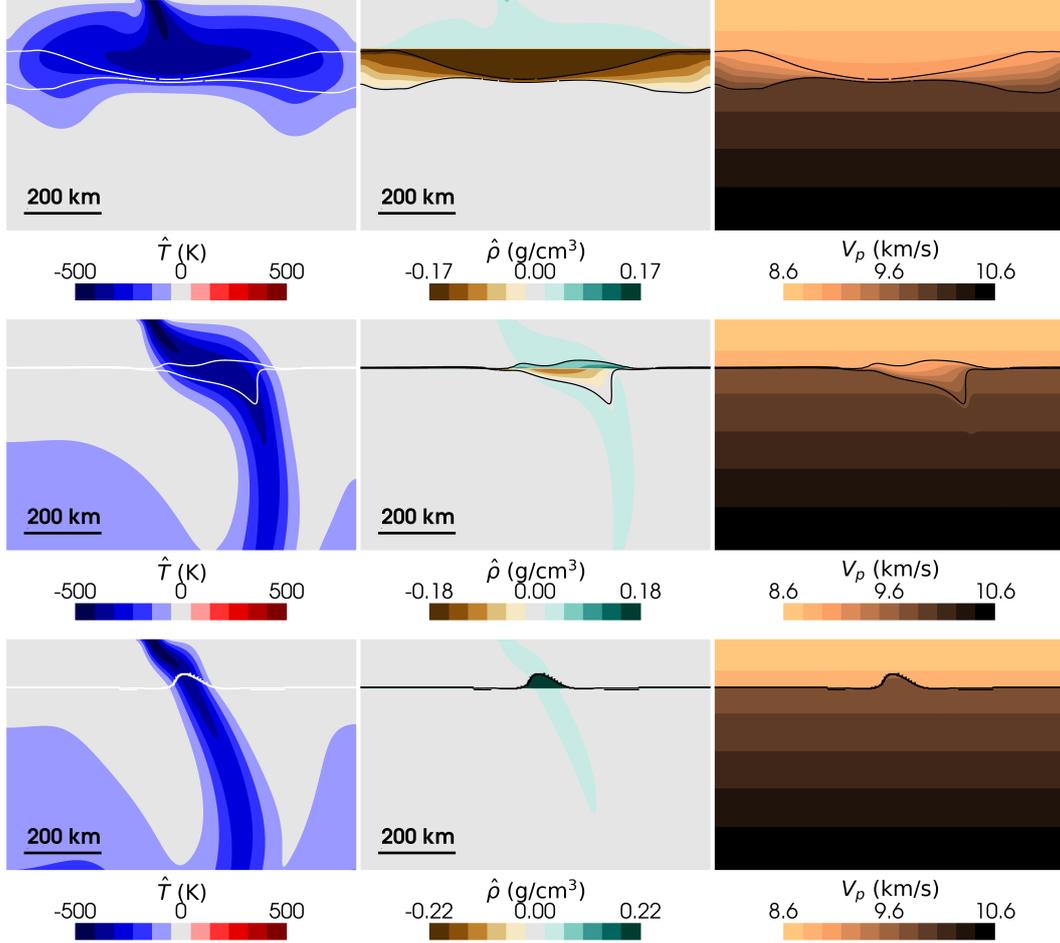


Figure 5: Slab simulations with intermediate strength contrasts ($B = 4$, viscosity contrast $\sim 3\times$) showing ultra-sluggish (top row: $Z = 3.0e0 \text{ K s}^{-1}$), intermediate (middle row: $Z = 4.7e2 \text{ K s}^{-1}$), and quasi-equilibrium (bottom row: $Z = 7.0e7 \text{ K s}^{-1}$) kinetic regimes after 100 Ma evolution. Panels show dynamic temperature \hat{T} (left column), dynamic density $\hat{\rho}$ (middle column), and pressure-wave velocity V_p (right column). Thin lines highlight the 10% and 90% wadsleyite volume fraction contours ($X = 0.1$ and 0.9). The 410 displacement is defined as the difference between the depth at $X = 0.9$ and the nominal equilibrium olivine \Leftrightarrow wadsleyite transition depth, while the 410 width is defined as the difference between depths at $X = 0.9$ and $X = 0.1$ (see Supplementary Information for details).

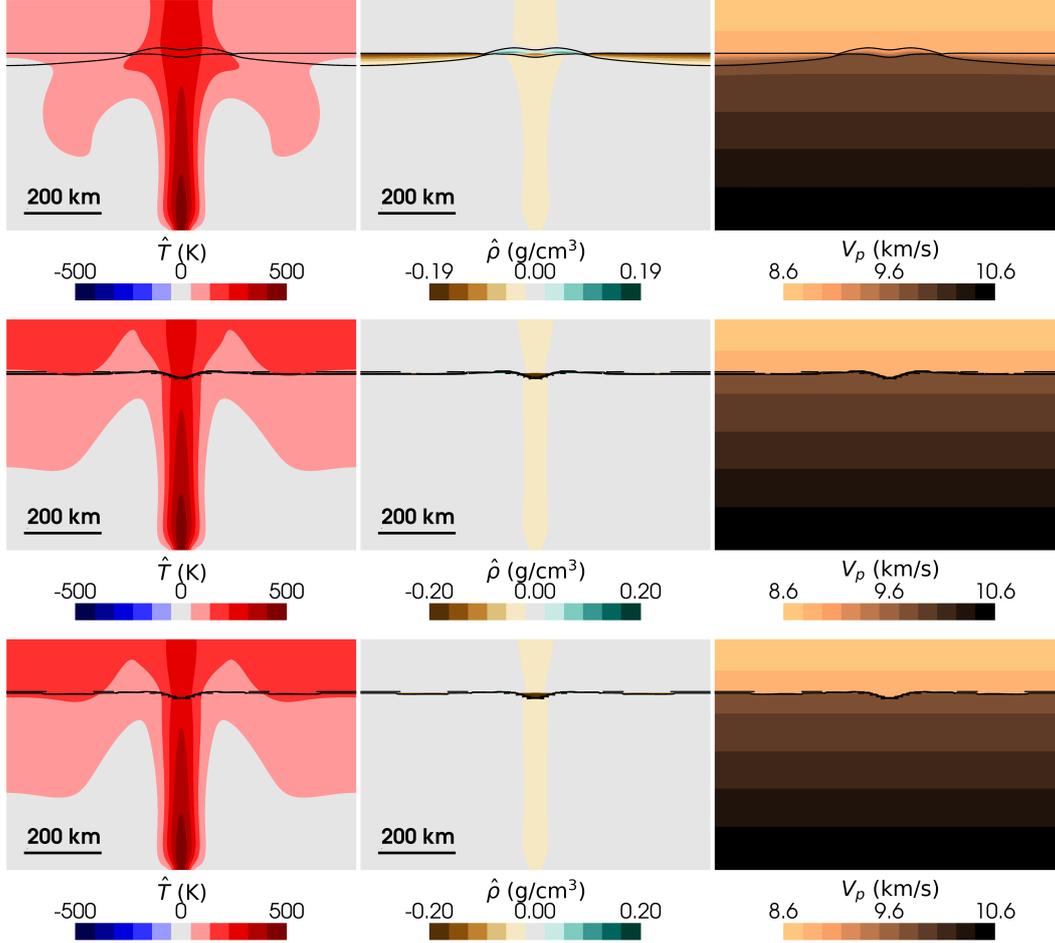


Figure 6: Plume simulations with intermediate strength contrasts ($B = 4$, viscosity contrast $\sim 1/3\times$) showing ultra-sluggish (top row: $Z = 3.0e0 \text{ K s}^{-1}$), intermediate-sluggish (middle row: $Z = 4.7e2 \text{ K s}^{-1}$), and quasi-equilibrium (bottom row: $Z = 7.0e7 \text{ K s}^{-1}$) kinetic regimes after 100 Ma evolution. Panels show dynamic temperature \hat{T} (left column), dynamic density $\hat{\rho}$ (middle column), and pressure-wave velocity V_p (right column). Thin lines highlight the 10% and 90% wadsleyite volume fraction contours ($X = 0.1$ and $X = 0.9$). The 410 displacement is defined as the difference between the depth at $X = 0.9$ and the nominal equilibrium olivine \leftrightarrow wadsleyite transition depth, while the 410 width is defined as the difference between depths at $X = 0.9$ and $X = 0.1$ (see Supplementary Information for details).

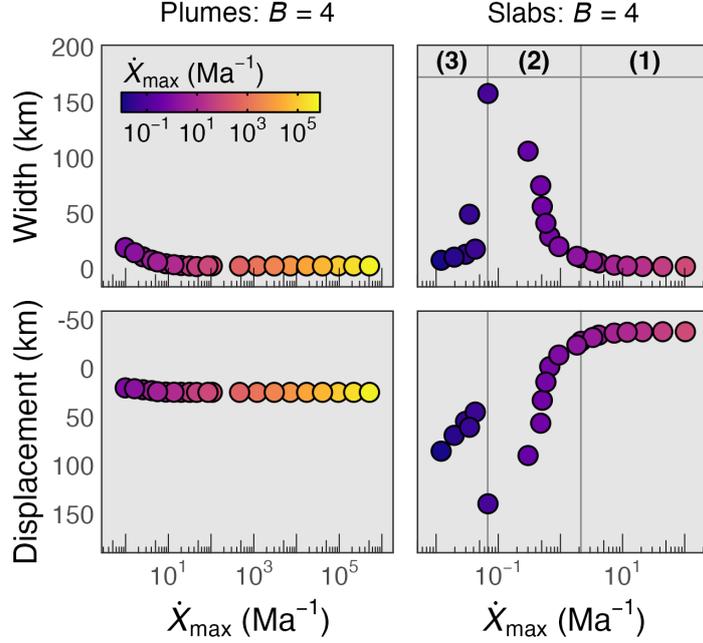


Figure 7: Measured 410 displacement and width versus maximum reaction rates \dot{X}_{\max} in plume and slab simulations with intermediate strength contrasts ($B = 4$) after 100 Ma. Structure of the 410 near plumes (left column) shows minimal dependence on \dot{X}_{\max} , with both displacement and width remaining nearly constant across seven orders of magnitude variation in \dot{X}_{\max} . In contrast, 410 structure near slabs (right column) changes distinctly across three kinetic regimes: (1) quasi-equilibrium at high \dot{X}_{\max} , where 410 widths are narrow and elevated; (2) an intermediate regime where decreasing reaction rates \dot{X}_{\max} progressively widen and deepen the 410; and (3) an ultra-sluggish regime at low \dot{X}_{\max} , where the 410 narrows while deepening, and slabs completely stall and pond.

395 At the lowest reaction rates ($Z \lesssim 2.0e2 \text{ K s}^{-1}$; $\dot{X}_{\text{max}} \lesssim 0.07 \text{ Ma}^{-1}$), a third kinetic
 396 regime emerges. While the 410 is displaced downwards, its width narrows with further
 397 reductions in \dot{X}_{max} . This ultra-sluggish kinetic regime reflects a transition to strong dis-
 398 equilibrium conditions and complete slab stagnation. As metastable olivine ponds and
 399 is pushed deeper, increasing pressure drives growing thermodynamic disequilibrium, even-
 400 tually triggering rapid transformation within a narrow depth range while surrounding
 401 regions remain kinetically frozen. The apparent 410 sharpening results from this pressure-
 402 controlled reaction front; only material pushed sufficiently deep accumulates enough ther-
 403 modynamic driving force to react, producing a sharp seismic discontinuity where this
 404 critical pressure is reached.

405 Rheological strength contrasts substantially modulate slab dynamics and 410 struc-
 406 ture through interactions with kinetic effects (Figure 8). Higher B values in Equation
 407 18 increase the viscosity contrast between the cold slab and surrounding mantle, pro-
 408 ducing a more coherent slab that penetrates the 410 with less internal deformation. Stronger
 409 slabs sink more sub-horizontally through the 410, limiting their vertical descent rates.
 410 Therefore, as B increases, the 410 sharpens because material traverses the phase tran-
 411 sition zone more slowly, allowing greater time for reaction progress despite sluggish ki-
 412 netics. In contrast, lower B values permit greater internal deformation and faster ver-
 413 tical descent, which amplifies kinetic effects and produces broader phase transition zones
 414 (see Supplementary Information for examples).

415 In summary, 410 structure near plumes is regulated by thermal effects near ther-
 416 modynamic equilibrium, whereas 410 structure near slabs exhibits distinct kinetic thresh-
 417 olds and non-linear scaling between its width, displacement, and the reaction rate \dot{X} .
 418 These contrasting behaviors underscore the differing roles of kinetics in hot versus cold
 419 mantle environments and imply that the 410 beneath slabs can transition abruptly be-
 420 tween thermodynamically- and kinetically-controlled regimes as reaction rates decrease.

421 **4 Discussion**

422 Our numerical simulations show that reaction kinetics exert a first-order control
 423 on the structure and seismic expression of the 410 discontinuity. The results presented
 424 in Section 3 demonstrate that plume and slab dynamics respond in systematically dif-
 425 ferent ways: plumes are insensitive to kinetics due to high temperatures, whereas slabs

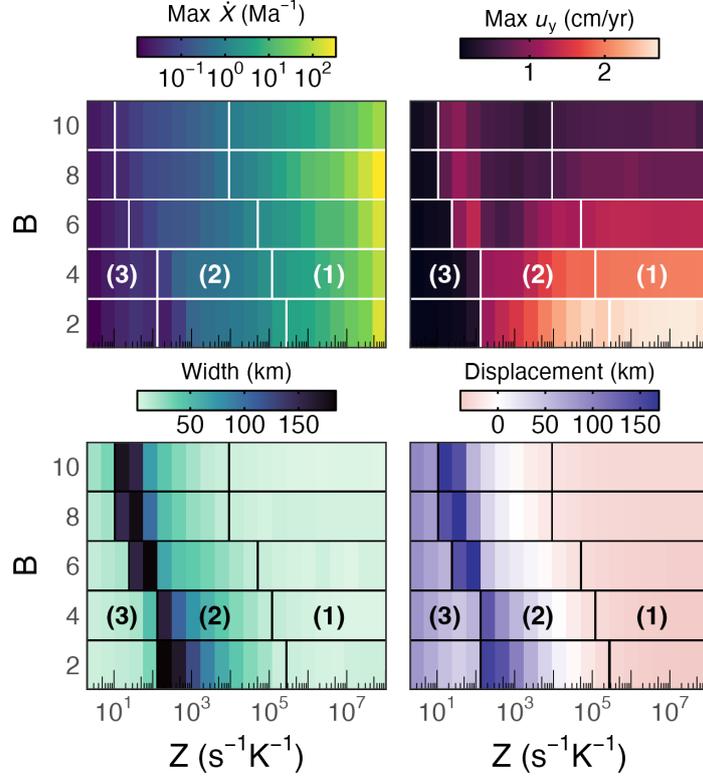


Figure 8: Variation in 410 structure and slab descent rate across kinetic and rheological regimes. Panels show maximum reaction rate (top left), maximum vertical velocity (top right), 410 width (bottom left), and 410 displacement (bottom right) as functions of the kinetic prefactor Z (horizontal axis, log scale) and rheological activation factor B (vertical axis). Each colored tile represents the measured value within a simulation after 100 Ma, and black/white lines delineate transitions between regime behaviors. The precise location of these transitions depends on B , where increasing rheological contrast progressively shifts the regime boundaries towards lower Z (more sluggish kinetic conditions). Text labels represent the observed kinetic regimes: (1) quasi-equilibrium, (2) intermediate, and (3) ultra-sluggish. The complete dataset is given in the Supplementary Information.

show three distinct kinetic regimes with thresholded behavior (Figure 7). Rheological strength contrasts, controlled by the activation factor B , further modulate these kinetic effects by altering slab geometry and descent rate (Figure 8). The implications of such contrasting relationships in slabs versus plumes are discussed below.

4.1 Uncertainties and Model Limitations

The primary quantitative uncertainty in our analysis stems from the kinetic prefactor Z in the interface-controlled olivine \Leftrightarrow wadsleyite growth model (Equation 13), which spans several orders of magnitude reflecting variable water contents (50–5000 ppm) and grain sizes (1–10 mm). Laboratory studies also reveal large uncertainties in kinetic parameters n , Γ , H^* , and V^* that depend strongly on water content, grain size, Mg-Fe composition, and microstructural evolution (Hosoya et al., 2005; Kubo et al., 2004; Ledoux et al., 2023; Liu et al., 1998; Perrillat et al., 2013; Rubie & Ross II, 1994). Our simulations therefore explore only a limited subset of potential reaction rates in Earth’s upper mantle.

Our kinetic model also assumes instantaneous nucleation site saturation followed by interface-controlled growth (Equations 9–13), thereby neglecting nucleation kinetics. While often justified because nucleation rates occur too rapidly for reliable measurement (Faccenda & Dal Zilio, 2017; Hosoya et al., 2005; Kubo et al., 2004; Perrillat et al., 2016), recent in-situ X-ray and acoustic studies (Ledoux et al., 2023; Ohuchi et al., 2022) document complex nucleation-growth microstructures that can limit net reaction rates under some PT conditions. By assuming saturated nucleation, we generally overestimate reaction rates and consequently underestimate the degree of olivine metastability and its influence on flow dynamics and 410 structure.

Beyond these kinetic uncertainties, our simulations incorporate several compositional and rheological simplifications. Assuming pure Mg endmembers neglects Fe-partitioning and minor element effects that can shift equilibrium depths by ~ 10 –20 km and alter kinetics (Katsura et al., 2004; Perrillat et al., 2016, 2013). We also neglect non-hydrostatic stress effects on microstructures and solid-state reactions (Wheeler, 2014, 2018, 2020). Our simple temperature-dependent viscosity (Equations 15–18) omits several strain-dependent processes that could affect both flow dynamics and reaction kinetics. Notably, accumulated strain could influence 410 topography through multiple pathways: grain size re-

duction would accelerate kinetics by increasing nucleation site density (affecting N in Equation 12), strain localization could similarly create zones of enhanced reaction rates, and strain-weakening could modify slab descent trajectory and residence time in the transition zone. While incorporating strain-weakening rheologies, grain-size evolution, and plastic deformation would provide a more complete treatment (S. Karato, Riedel, & Yuen, 2001), such additions would substantially expand an already large parameter space and introduce additional uncertainties in constitutive relationships.

Finally, our 2D simulations neglect 3D slab geometry and dynamics. While we expect the same kinetic regimes to occur in 3D, the transitions between regimes will likely shift as slabs behave differently in 3D versus 2D (Sime, Wilson, & van Keken, 2024). Despite these combined limitations in kinetic parameters, compositional complexity, rheological formulation, and dimensionality, our results capture first-order effects governing 410 structure.

4.2 Implications for Subduction Dynamics

The three kinetic regimes identified in our slab simulations—quasi-equilibrium, intermediate, and ultra-sluggish—emerge from feedbacks between kinetically controlled phase transitions and slab strength (Figure 8). However, seismic tomography shows little to no evidence for widespread slab ponding at the 410 (Fukao & Obayashi, 2013), providing an observational constraint on plausible kinetic behavior in natural systems. In particular, the ultra-sluggish regime ($\dot{X} \lesssim 0.07 \text{ Ma}^{-1}$), which leads to complete slab stagnation at the 410 in our simulations, is inconsistent with global seismic observations of continuous slab descent through the 410. This implies that most subduction zones experience sufficiently rapid olivine \leftrightarrow wadsleyite transformation to avoid long-lived stagnation and ponding at the 410.

Meanwhile, the occurrence of deep earthquakes often attributed to transformational faulting could indicate metastable olivine persistence in various subduction zones (H. Green & Houston, 1995; Ishii & Ohtani, 2021; Kirby et al., 1996; Ohuchi et al., 2022; Sindhusuta et al., 2025) and thus be compatible with the intermediate kinetic regime in our simulations ($0.07 \lesssim \dot{X} \lesssim 2.2 \text{ Ma}^{-1}$). This regime would generate localized buoyant regions that resist but do not prevent downward flow. Assuming that transformational faulting is primarily responsible for deep earthquakes, rather than alternative mechanisms (e.g.,

488 Zhan, 2020), our simulations suggest that coexistence of deep seismicity with continu-
 489 ous slab descent through the 410 requires a delicate balance: olivine \leftrightarrow wadsleyite re-
 490 action rates must be slow enough to sustain metastable volumes for transformational fault-
 491 ing, yet fast enough to permit 410 penetration.

492 Rheological contrasts further modulate these kinetic effects by controlling slab tra-
 493 jectory and descent rate. Strong slabs ($B \gtrsim 6$, viscosity contrast $\sim 6\text{--}20\times$) maintain co-
 494 herence and penetrate sub-horizontally, spending more time within the phase transition
 495 zone where olivine transforms more completely. Weaker slabs ($B \lesssim 6$, viscosity contrast
 496 $\sim 2\text{--}6\times$) deform internally and descend vertically, traversing the transition zone quickly
 497 with less time for sluggish reactions. This morphological dependence on slab strength
 498 is consistent with previous numerical studies without reaction kinetics (Garel et al., 2014),
 499 indicating that rheological control of slab geometry operates independently of kinetic ef-
 500 fects.

501 Considering both kinetic and rheological influences can produce counterintuitive
 502 subduction dynamics, however. Under equivalent kinetic conditions, our simulations show
 503 stronger slabs descending through the 410, while weaker slabs accumulate more metastable
 504 olivine, amplifying buoyancy forces that slow or arrest downward slab motion. This out-
 505 come appears contradictory to previous work linking deep earthquakes with colder, stronger
 506 slabs (H. Green & Houston, 1995; Houston, 2015; Zhan, 2020), suggesting that other factors—
 507 such as overriding plate forcing or subduction geometry (e.g., Agrusta et al., 2017)—may
 508 dominate over kinetics in natural systems.

509 Our slab simulations also reveal a systematic departure from observed descent rates
 510 across the current global subduction system. Simulated slabs descend at 1.3–2.0 cm/yr
 511 (interquartile range excluding fully stagnated cases; see Supplementary Information), roughly
 512 half of the range compiled by Lallemand, Heuret, and Boutelier (2005) for natural sys-
 513 tems (interquartile range: 2.6–4.8 cm/yr). This discrepancy suggests that buoyancy forces
 514 from metastable olivine accumulation may be exaggerated in our simulations relative to
 515 Earth, although faster descent rates observed in natural subduction zones should am-
 516 plify metastability if kinetic rates are sluggish.

517 Furthermore, our simulations point to a critical kinetic threshold near $\dot{X} \sim 0.07$
 518 Ma^{-1} that marks where buoyancy forces from incomplete olivine \leftrightarrow wadsleyite trans-
 519 formation either prevent or permit downward slab motion. This narrow threshold shifts

520 with slab strength, where coherent slabs penetrate the 410 at reaction rates that would
 521 stall weaker slabs (Figure 8). These dynamic sensitivities suggest individual subduction
 522 zones could oscillate between penetration and temporary stagnation at the 410 as kine-
 523 matic and PT conditions evolve, with plate forcing and slab deformation behavior (e.g.,
 524 Agrusta et al., 2017) potentially modulating this critical kinetic threshold.

525 Regional variability in slab behavior (Fukao & Obayashi, 2013) could therefore re-
 526 flect diversity in both kinetics and rheology, in addition to slab age and convergence rate.
 527 In our simulations, young, hot slabs with lower viscosity contrasts descend steeply and
 528 accumulate moderate metastable olivine despite warm thermal structures, while old, cold
 529 slabs with high viscosity contrasts flatten and sink slowly, allowing near-complete trans-
 530 formation under moderately sluggish kinetics. These patterns distinguish slabs from plumes:
 531 in hot upwellings, elevated temperatures suppress sensitivity to both kinetics and rhe-
 532 ology, while in cold slabs, kinetics govern reaction rates and rheology dictates reaction
 533 duration by regulating slab kinematics. Accurately modeling slab morphology, material
 534 exchange, and deep stress conditions in geodynamic simulations therefore requires in-
 535 corporating both effects.

536 **4.3 Implications for 410 Detectability and Constraining Kinetics and** 537 **Rheology from Seismic Observations**

538 The 410 discontinuity is readily detected using underside reflections (precursors to
 539 SS, PP, and ScS reverberated phases), as well as converted phases, (receiver functions),
 540 and top-side triplicated phases (e.g., Chambers et al., 2005; Cottaar & Deuss, 2016; Deuss,
 541 2009; Flanagan & Shearer, 1999; Glasgow et al., 2024; Han et al., 2021; Houser & Williams,
 542 2010; Jenkins et al., 2016; Miao, Gao, Sun, & Liu, 2024; Parera-Portell, Mancilla, Morales,
 543 & Díaz, 2024; Schmerr & Garnero, 2007; Shearer, 2000; Wang, Li, & Chen, 2017; Waszek,
 544 Anandawansha, Sexton, & Tauzin, 2024). The majority of studies focus on mapping 410
 545 topography, and typically assume a sharp near-horizontal interface. Resolving the width
 546 of the phase transition zone requires more challenging analyses, including constraints on
 547 impedance contrast. However, the trade-off between phase transition width, impedance
 548 contrast, and small-scale topography depends strongly on the wavelengths of the seis-
 549 mic phases employed (Chambers et al., 2005).

550 Previous studies have exploited the frequency dependence of observed amplitudes
 551 (e.g., Bonatto, Piromallo, & Cottaar, 2020; Van der Meijde, Marone, Giardini, & Van der
 552 Lee, 2003), the detectability of discontinuities at higher frequencies (e.g., Day & Deuss,
 553 2013; Rost & Weber, 2002), gradient-based inversions (Schmandt, 2012), and joint anal-
 554 yses of top- and bottom-side reflections (Vinnik et al., 2020). In many of these approaches,
 555 the transition is parameterized as a simple linear gradient, whereas our models predict
 556 a more complex depth-dependent gradient, consistent with results from gradient-based
 557 inversions (Schmandt, 2012). While many of these studies infer a sharp 410, locally broader
 558 phase transitions, up to 35 km, are observed and are commonly attributed to elevated
 559 water content in the mantle (e.g., Schmandt, 2012; Van der Meijde et al., 2003; Vinnik
 560 et al., 2020).

561 The presence of water is expected to significantly widen the olivine \Leftrightarrow wadsleyite
 562 transition width, similar to effects observed in our simulations. However, a hydrous 410
 563 transition would likely occur at lower pressures (Smyth & Frost, 2002), while our sim-
 564 ulation results show a deepening of the discontinuity for the intermediate kinetic regime
 565 with an inhibited olivine \Leftrightarrow wadsleyite transformation. Therefore, resolving topography
 566 could be a means to distinguish these two scenarios.

567 Our plume simulations predict consistently thin 410 discontinuities (2–3 km widths,
 568 ~ 24 km displacements) across large rheological variations and seven orders of magnitude
 569 in \dot{X} , except under ultra-sluggish kinetics where widths broaden up to 21 km. These sharp
 570 discontinuities should be readily detectable, consistent with observations of well-defined
 571 410s with strong deflections in various hotspot locations (Deuss, 2009; Lawrence & Shearer,
 572 2008). Conversely, the local absence of a detectable 410 has been reported near Hawaii
 573 (Kemp, Jenkins, MacLennan, & Cottaar, 2019) and attributed to the potential accumu-
 574 lation of basalt.

575 Slab simulations, in contrast, imply that 410 detectability strongly depends on joint
 576 kinetic and rheological influences (Figure 8). Strong slabs ($B \gtrsim 6$, viscosity contrast ~ 6 –
 577 $20\times$) descending slowly along sub-horizontal trajectories in our simulations maximize
 578 residence time in the phase transition zone, producing sharp, detectable 410 signals due
 579 to near-complete olivine \Leftrightarrow wadsleyite transformation. Weak slabs ($B \lesssim 6$, viscosity con-
 580 trast ~ 2 – $6\times$) descending steeply with reduced residence times amplify kinetic inhibition,
 581 producing broader reaction fronts. Weakened 410 signals beneath some subduction zones

582 (Van Stiphout, Cottaar, & Deuss, 2019), or observations of low velocity regions possi-
583 bly representing metastable olivine (Han et al., 2021; Jiang, Zhao, & Zhang, 2015; Shen
584 & Zhan, 2020), align with intermediate kinetic conditions and relatively weak slabs, where
585 steep, rapid descent amplifies metastability.

586 Understanding the joint influence of rheological and kinetic factors on the geom-
587 etry and dynamics of slab descent and phase transition width will offer a quantitative
588 framework for interpreting observed seismic structure. Kinetic factors could potentially
589 lead to significantly extended phase transition zones, perhaps preventing detection of the
590 410 by lower frequency seismic phases such as SS precursors. However, these anomalies
591 are predicted to occur over narrow regions where slabs interact with the 410 (Figure 5).
592 Thus, finer-scale topographic mapping with higher frequency phases, such as receiver func-
593 tions is likely needed to localize non-detectability (Van Stiphout et al., 2019).

594 In principle, regional variations in both 410 topography and phase transition width
595 could reflect variations in kinetics (through temperature, composition, water content, or
596 grain size), variations in rheology (through additional effects like accumulated strain),
597 or compensating variations in both. Without multiple independent constraints, seismic
598 observations of 410 structure alone cannot uniquely separate these effects. Examples for
599 independent constraints may include the presence of deep seismicity, as well as variations
600 in slab thermal structure, age, and hydration across subduction zones (Agius, Rychert,
601 Harmon, & Laske, 2017; Schmandt, 2012; Van Stiphout et al., 2019).

602 Forward modeling of seismically observable 410 width and topography enables test-
603 ing of whether specific parameter combinations match observed 410 structure from re-
604 ceiver functions or precursors. However, until mineral physics experiments (e.g., Hosoya
605 et al., 2005; Kubo et al., 2004; Ledoux et al., 2023; Perrillat et al., 2016, 2013) reduce
606 uncertainties and the issue of parameter degeneracy has been sufficiently mitigated through
607 independent constraints, seismic observations provide order-of-magnitude estimates of
608 effective \dot{X} and relative rheological strength. Nevertheless, the threshold behavior and
609 scaling relationships from our simulations demonstrate that comprehensive multi-observation
610 approaches are essential for constraining micro-scale processes governing phase transi-
611 tions and their geodynamic consequences.

5 Conclusions

The olivine \Leftrightarrow wadsleyite phase transition and resulting 410 structure are strongly influenced by the combined effects of reaction kinetics and rheological strength on flow dynamics. We quantified these effects by integrating an interface-controlled olivine \Leftrightarrow wadsleyite growth model with compressible simulations of mantle plumes and slabs, systematically exploring kinetic factors spanning seven orders of magnitude. Each simulation was evaluated across a large range of viscosity contrasts and 410 structure was determined after 100 Ma.

Our results reveal fundamentally different responses in hot versus cold environments. Plumes produce consistently sharp discontinuities (2–3 km wide) across the entire parameter space, implying that seismic observations beneath hotspots primarily constrain thermal structure near thermodynamic equilibrium rather than kinetic or rheological parameters. Slabs exhibit distinct threshold behavior across three kinetic regimes—quasi-equilibrium, intermediate, and ultra-sluggish—that are further modulated by viscosity contrasts controlling slab geometry and transit time through the phase transition zone.

Widespread slab penetration of the 410 in seismic tomography (Fukao & Obayashi, 2013) requires effective reaction rates exceeding the ultra-sluggish kinetic regime ($\dot{X} \gtrsim 0.07 \text{ Ma}^{-1}$). This critical threshold shifts systematically with rheological strength, revealing that modest variations in either reaction rates or viscosity contrasts can produce substantial diversity in observed 410 topography. Uniquely constraining kinetic versus rheological contributions requires combining 410 structural observations with independent constraints from high-resolution tomography and kinematic data (providing descent geometry) and deep seismicity patterns (indicating metastable olivine volumes).

The 410 can therefore serve as a seismological probe of kinetic conditions in cold subduction environments where disequilibrium effects are amplified. Realizing this potential requires reducing uncertainties through targeted mineral physics experiments that better quantify nucleation versus growth mechanisms, water and compositional effects on reaction rates, and microstructural evolution during deformation. Integrating such constraints with high-resolution seismic imaging and the forward modeling framework presented here offers a pathway toward understanding how micro-scale kinetic processes govern mantle convection and shape Earth’s interior seismic structure.

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650 **Data Availability**

651 All data, code, and relevant information for reproducing this work can be found
652 at https://github.com/buchanankerswell/kerswell_et_al_410_kinetics, and at <https://doi.org/10.17605/OSF.IO/9PHWC>, the official Open Science Framework data repository.
653 All code within these repositories is MIT Licensed and free for use and distribution (see
654 license details). ASPECT version 3.0.0, (Bangerth et al., 2024a, 2024b; Clevenger & Heis-
655 ter, 2021; Fraters, 2020; Fraters et al., 2019; Gassmöller et al., 2018; Heister et al., 2017;
656 Kronbichler et al., 2012) used in these computations is freely available under the GPL
657 v2.0 or later license through its software landing page [https://geodynamics.org/resources/](https://geodynamics.org/resources/aspect)
658 [aspect](https://aspect.geodynamics.org) or <https://aspect.geodynamics.org> and is being actively developed on GitHub
659 and can be accessed via <https://github.com/geodynamics/aspect>.
660

661 **Conflict of Interest**

662 The authors declare there are no conflicts of interest for this manuscript.

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